



SpaceX Propulsion

Tom Markusic
Space Exploration Technologies

46th AIAA/ASME/SAE/ASEE
Joint Propulsion Conference
July 28, 2010



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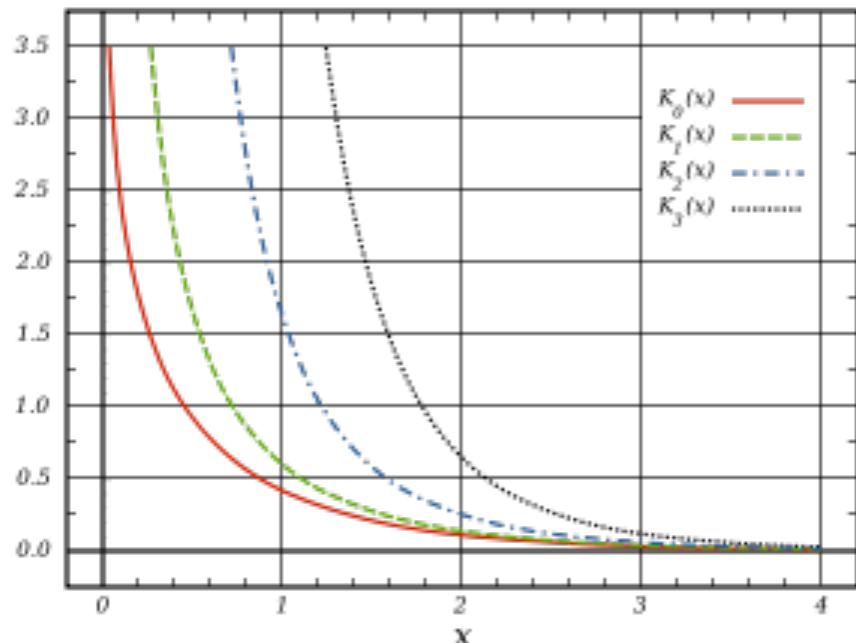
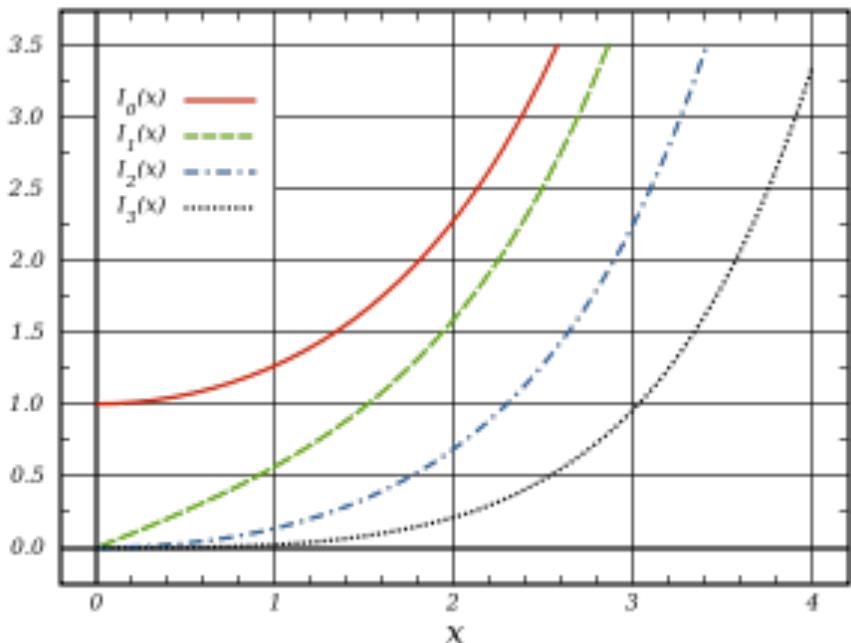
Inverse Hyperbolic Bessel Functions

$$x^2 \frac{d^2y}{dx^2} + x \frac{dy}{dx} - (x^2 + \alpha^2)y = 0.$$

$$I_\alpha(x) = i^{-\alpha} J_\alpha(ix) = \sum_{m=0}^{\infty} \frac{1}{m! \Gamma(m+\alpha+1)} \left(\frac{x}{2}\right)^{2m+\alpha}$$

$$K_\alpha(x) = \frac{1}{2} e^{-\frac{1}{2}\alpha\pi i} \int_{-\infty}^{+\infty} e^{-ix \sinh t - \alpha t} dt$$

$$K_\alpha(x) = \frac{\pi}{2} \frac{I_{-\alpha}(x) - I_\alpha(x)}{\sin(\alpha\pi)} = \frac{\pi}{2} i^{\alpha+1} H_\alpha^{(1)}(ix) = -\frac{\pi}{2} i^{\alpha+1} e^{-i\pi\alpha} H_\alpha^{(2)}(-ix).$$



Near-term Propulsion Needs

McGregor Rocket Development Facility



Near-term Propulsion Needs

**J-2X**

HLLV Propulsion

- Merlin 2 uses scaled-up, flight proven Merlin 1 design
- SpaceX can develop and flight qualify the Merlin 2 engine in ~3 years at a cost of ~\$1B.
Production: ~\$50M/engine
- J-2X development already in progress under Constellation program

| | Merlin 2 | I-2X |
|---------------------|----------|---------------------|
| Propellant | LOX/RP | LOX/LH ₂ |
| Thrust (vac) [klbf] | 1,700 | 292 |
| Isp (vac) [sec] | 322 | 448 |
| T/W [lbf/lbm] | 150 | 55 |

**Merlin 2**

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Solar Electric Propulsion for Cargo Tug



NEXT
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Busek BHT-20K
Hall Thruster

NASA 457M
Hall Thruster

- Cluster of ~5 high TRL thrusters process 100 kWe solar power
- Next generation tug uses single high power thruster, such as NASA 457M
- Third generation tug uses nuclear electric propulsion at megawatt levels

| | NEXT | BHT-20 | 457M |
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| Thrust [mN] | 236 | 1080 | 3300 |
| Isp [sec] | 4100 | 2750 | 3500 |
| Efficiency [%] | 70 | 72 | 58 |

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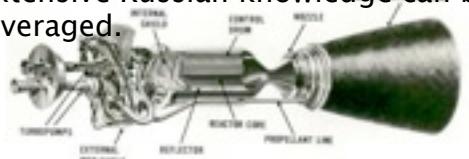
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Nuclear Thermal Propulsion for Mars



Stage

- NERVA stage technology
 - Total thrust ~ 60 klbf, using 2 to 6 NDR
 - Propellant: hydrogen, Isp ~ 930 sec
- ISRU or pre-deployed propellant for return mission
- Technology has been verified with >17 Hours of hot-fire tests, including restarts. No additional developmental, terrestrial tests (with nuclear) fuel are required.
- Extensive Russian knowledge can be leveraged.



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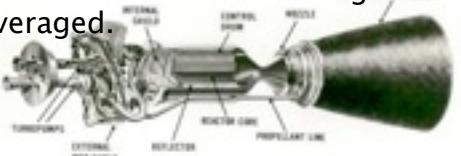
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LOX/Methane Propulsion for Ascent/Descent

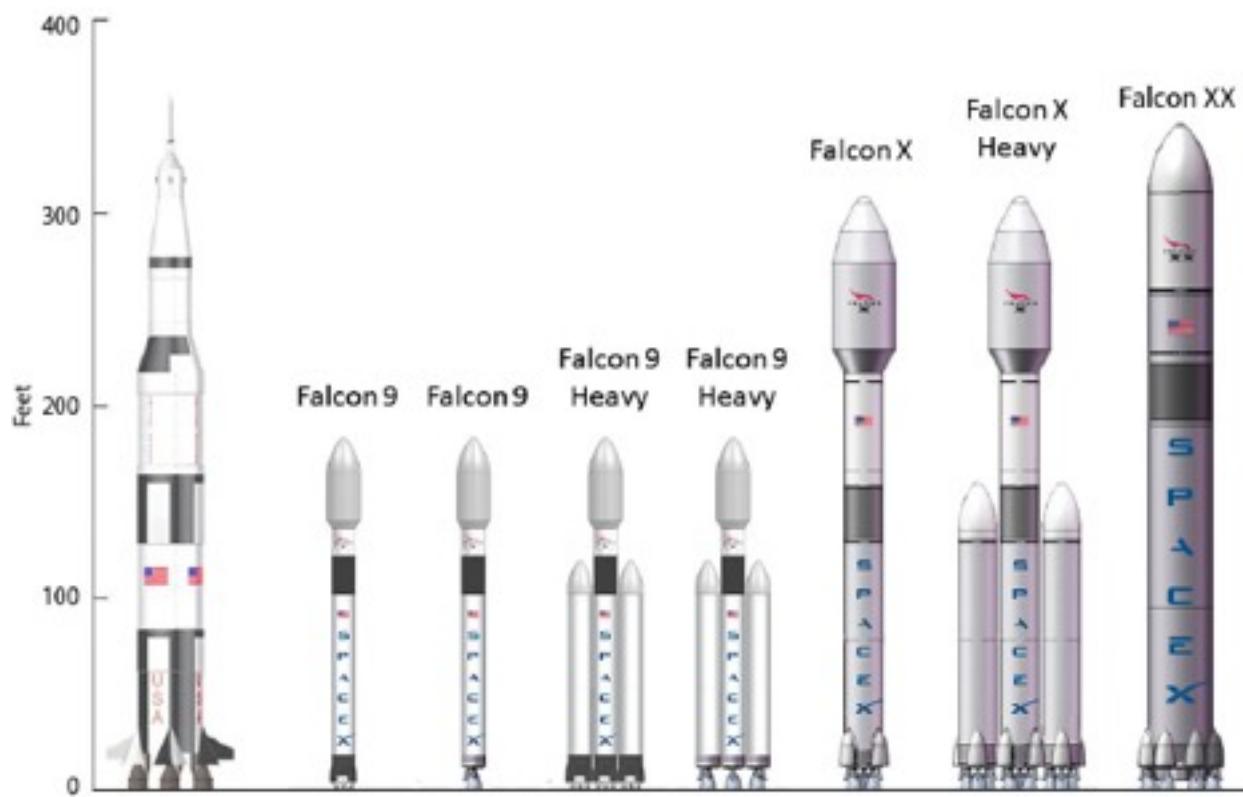
- ISRU-derived methane will be used for ascent/descent propulsion
- Strong developmental programs currently underway at Aerojet, ATK/XCOR
- SpaceX Merlin 1 engine may be reconfigurable to for LOX/methane, providing a large (~100 klbf) GG cycle engine for ascent/descent



Aerojet, T = 5.5 k-lbf, Isp = 350 sec



ATK/XCOR, T = 7.5 k-lbf, Isp = ?

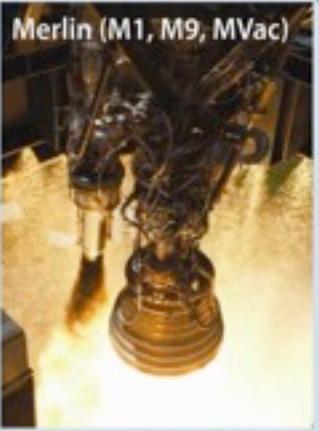


| VEHICLE | Falcon 9 | Falcon 9 | Falcon 9 Heavy | Falcon 9 Heavy | Falcon X | Falcon X Heavy | Falcon XX |
|--------------------------------|-----------|----------|----------------|----------------|----------|----------------|-----------|
| 1st Stage Engines | Merlin 1D | Merlin 2 | Merlin 1D | Merlin 2 | Merlin 2 | Merlin 2 | Merlin 2 |
| Core Diameter (meters) | 3.6 | 3.6 | 3.6 | 3.6 | 6 | 6 | 10 |
| Number of Cores | 1 | 1 | 3 | 3 | 1 | 3 | 1 |
| Engines per Core | 9 | 1 | 9 | 1 | 3 | 3 | 6 |
| Engine Thrust (sea level, lbf) | 120k | 1.2M | 120k | 1.2M | 1.2M | 1.2M | 1.7M |
| Total Lift-off Thrust (lbf) | 1.08M | 1.2M | 3.24M | 3.6M | 3.6M | 10.8M | 10.2M |
| Engine Out Capability? | Yes | No | Yes | No | Yes | Yes | Partial |
| Mass to LEO (kg) | 10.5k | 11.5k | 32k | 34k | 38k | 125k | 140k |

Testing Survey

Texas Test Site

Engine Testing



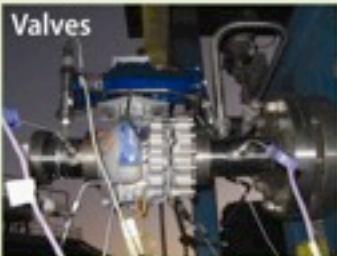
Stage Testing

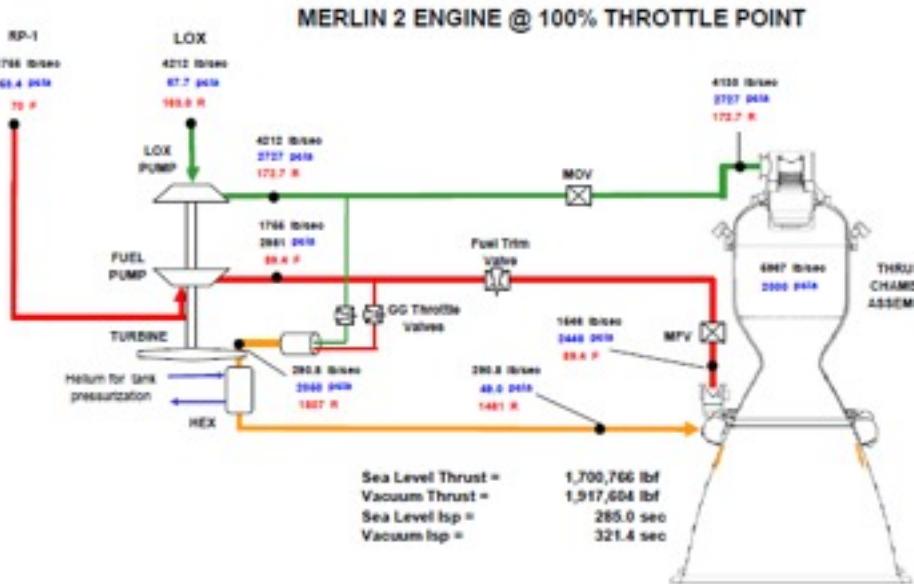


Structural Testing



Component Testing





| 100% RPL | |
|--------------|------------|
| RP1 Flowrate | 16,700 GPM |
| LOX Flowrate | 26,500 GPM |

Table 1: Merlin 2 Engine Summary

| Parameter | 70% Throttle Point | 100% Throttle Point |
|-------------------------|--------------------|---------------------|
| Propellants | LOX/RP-1 | LOX/RP-1 |
| Sea Level Thrust | 1.20M lbf | 1.70M lbf |
| Vacuum Thrust | 1.42M lbf | 1.92M lbf |
| Sea Level Isp | 271 seconds | 285 seconds |
| Vacuum Isp | 320 seconds | 325 seconds |
| Chamber Pressure | 1472 psia | 2000 psia |
| Nozzle Area Ratio | 25:1 | 25:1 |
| Mixture Ratio (Ox/fuel) | 2.4 | 2.4 |
| Throttle Setting | 70 % | 100 % |

Figure 12: Merlin 2

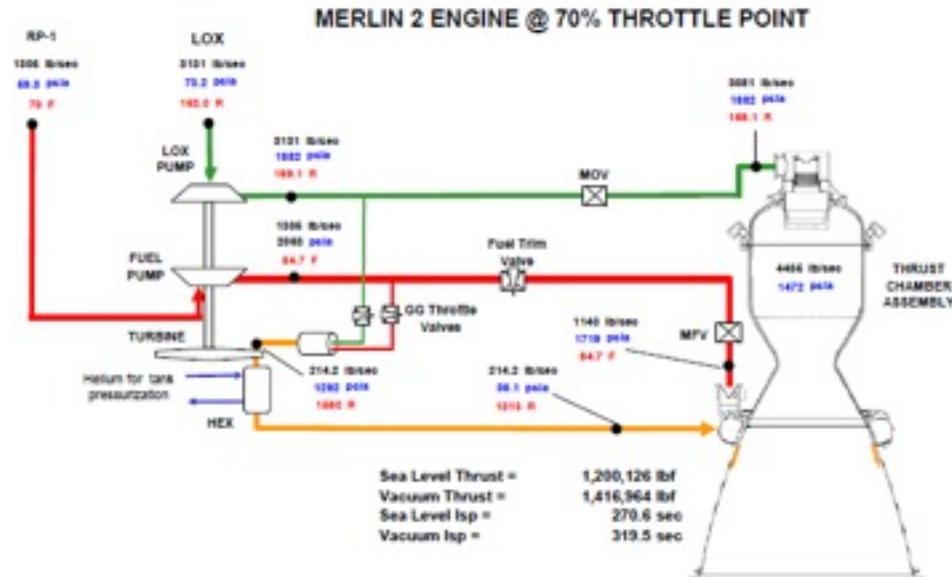
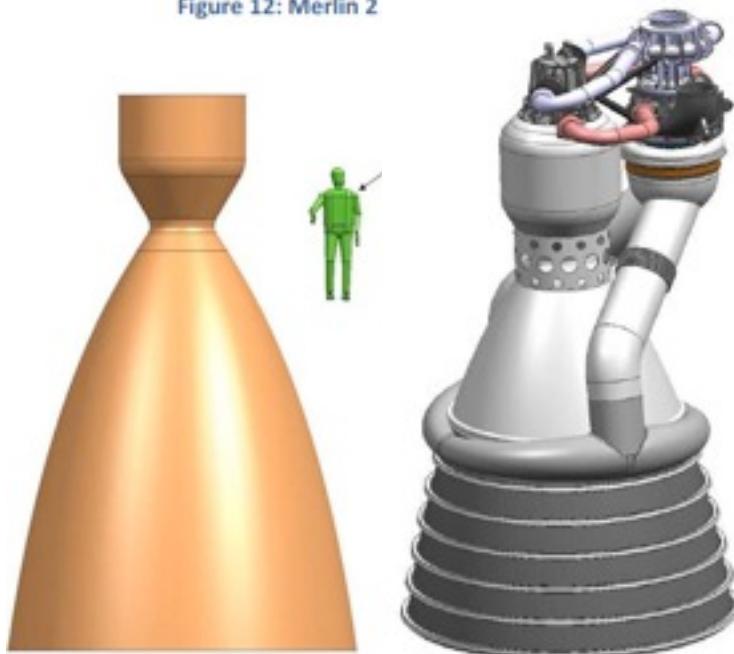


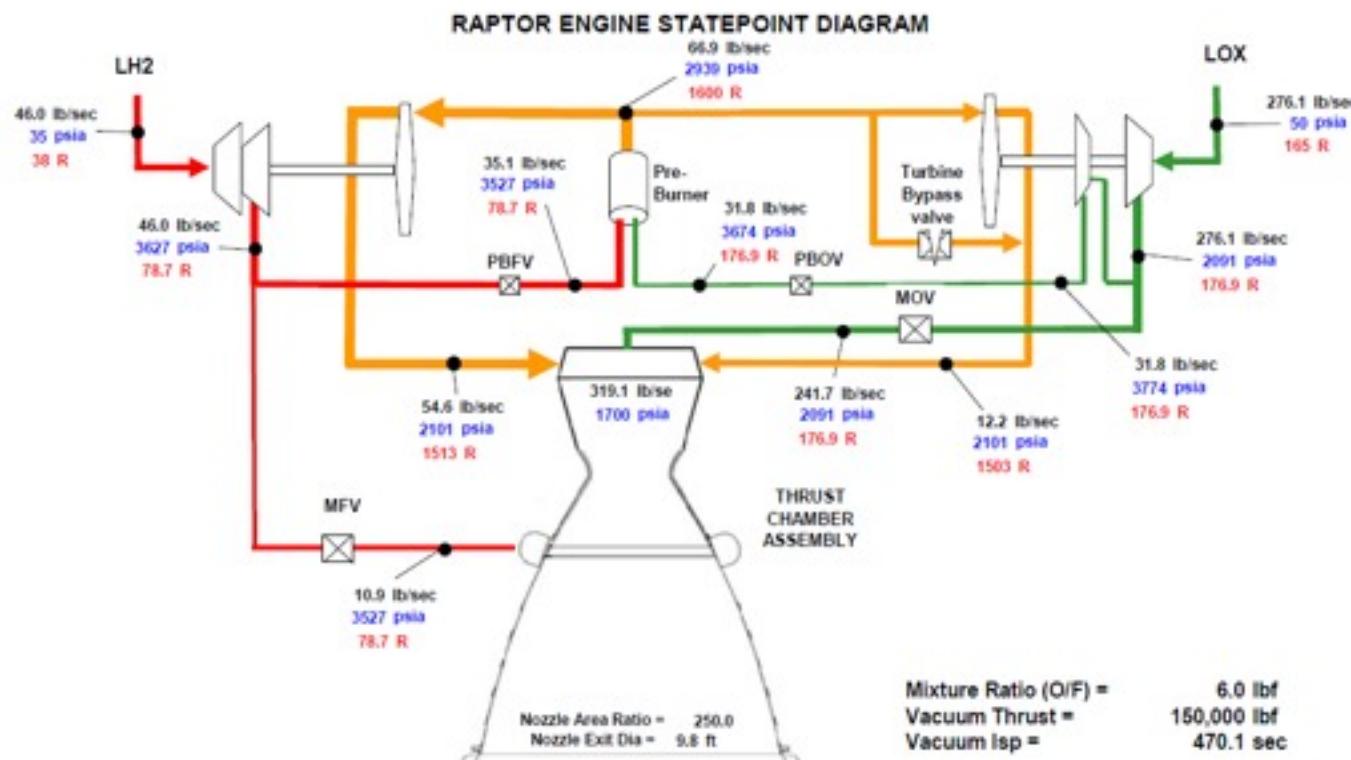
Figure 11: Merlin 2 State Point Diagram at 70% Throttle

SPACEX

Raptor



| Parameter | Value |
|-------------------------|---------------------|
| Propellants | LOX/LH ₂ |
| Vacuum Thrust | 150,000 lbf |
| Vacuum Isp | 470.1 seconds |
| Chamber Pressure | 1700 psia |
| Nozzle Area Ratio | 250:1 |
| Mixture Ratio (Ox/fuel) | 6.0 |
| Throttle Range | 50 - 100 % |

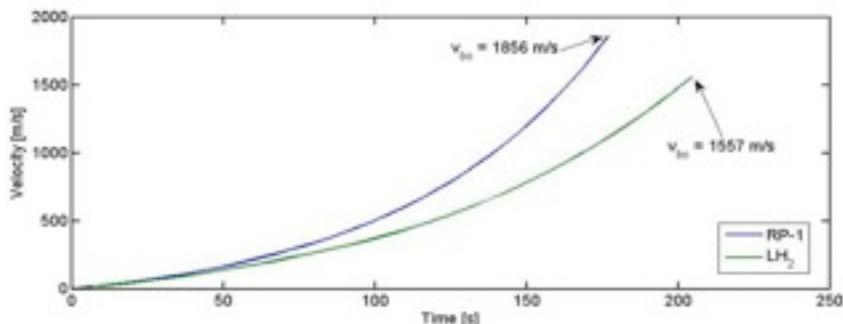
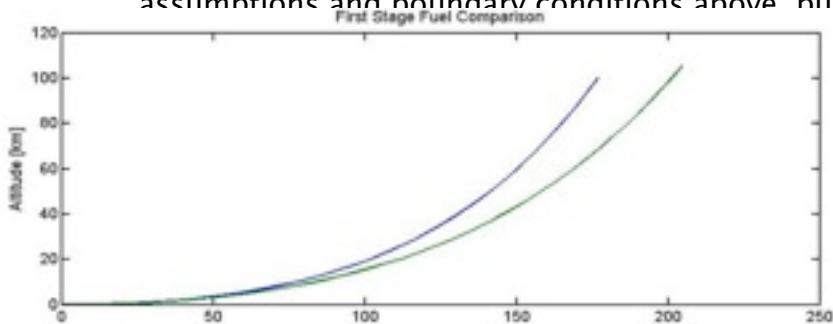




LOX/RP versus LOX/LH₂ Booster

Fundamentals

- Simple 1-D dynamic model used to compare LOX/RP and LOX/LH₂ first stage performance for a HLLV
 - First, for both propellants, propellant mass was chosen to yield the same ΔV (3.6 km/s) for a given payload (750 MT), consistent with Saturn V, but with no external forces.
 - Typical engine performance and tank mass fractions assumed.
 - Initial T/W fixed at 1.2 for both cases. Ballistic trajectory.
 - Equations of motion again integrated using assumptions and boundary conditions above, but

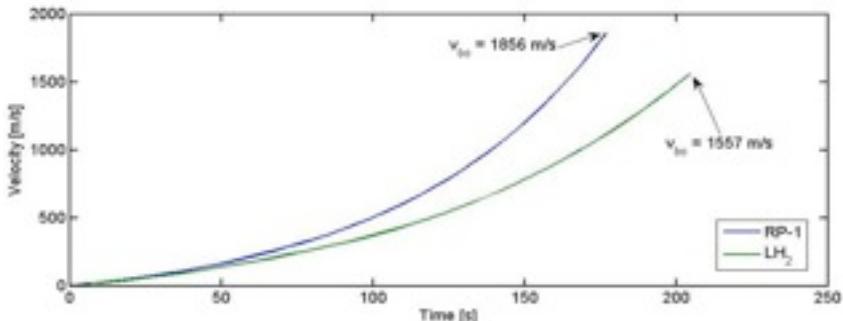
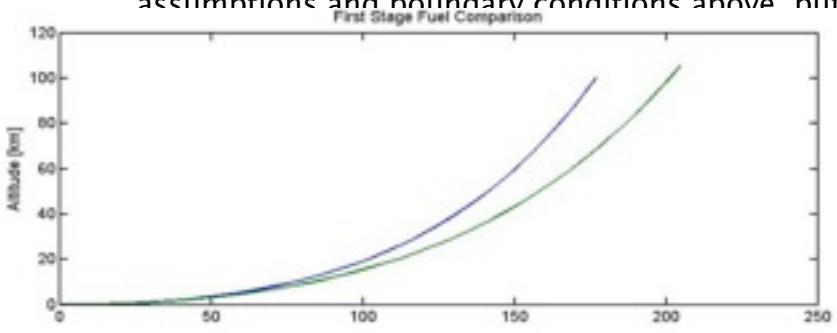




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Trade Studies

- Recent NASA-led "Heavy Lift Launch Vehicle Study" compared many configurations of LOX/LH₂, LOX/RP, SRB propulsion for a HLLV.
 - Configuration with 6 Lox/RP engine first stage competitive with all concepts in performance and mission capture metrics
 - Configuration with 6 Lox/RP engine first stage shown to provide benefits in safety and annual recurring cost metrics above all LOX/LH₂ and SRB

Operations

Handling

- configurations
- Deep cryogenic (-432 F) vs room temperature for RP
- LH₂ has high infrastructure investment for test and launch

Safety

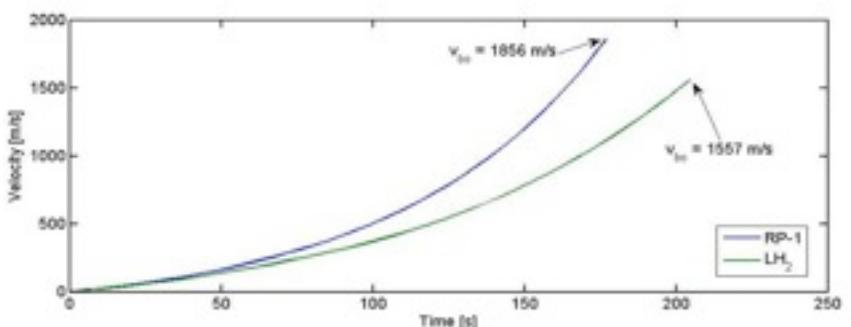
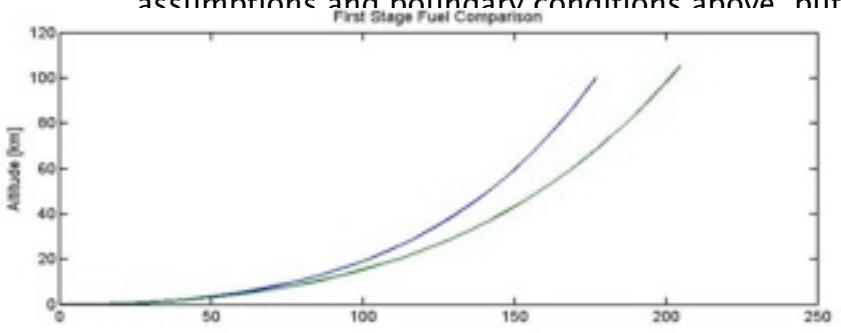
- LH₂ leaks lead to detonation risk—extensive monitoring required
- RP leaks are easily (visually) detectable, low explosion risk



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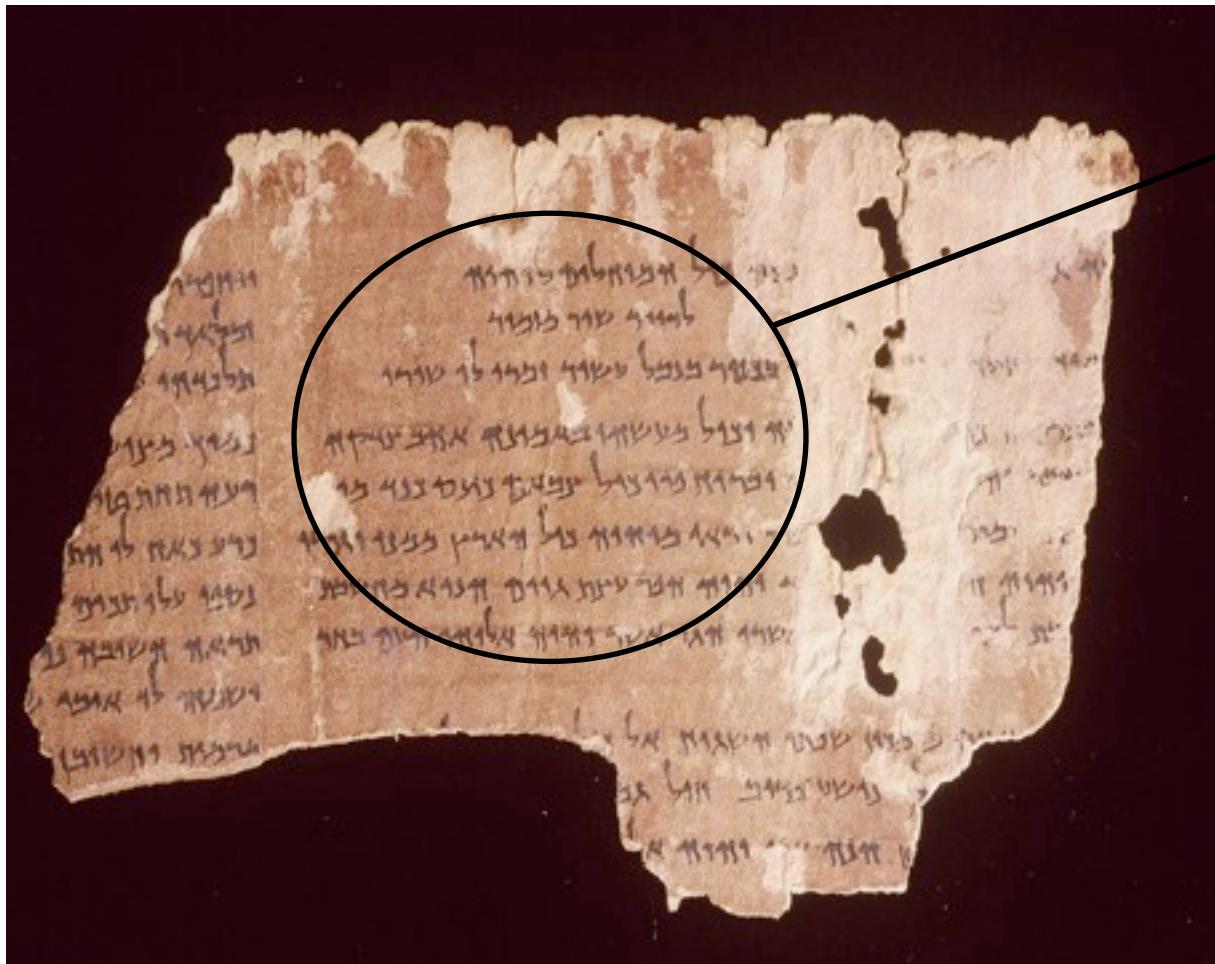
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- Safety.**
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RP staged combustion versus GG

- Cycle** stage ΔV simplified model compared Merlin 2 gas generator cycle engine with scaled up RS-84 derived staged combustion engine.
 - Mass of Merlin 2 based on current design (sea level thrust = 1.7 Mlbf). Mass of RS-84 derived engine estimated by linearly scaling thrust and assuming T/W is constant.
 - Merlin 2 vac Isp = 322.1 sec, RS-84 derived vac Isp = 334.6 sec.
 - Modeled Falcon X with F9 flight trajectory (250 km x 34.5 deg).
 - Found burnout velocity for Merlin 2 stage and RS-84 derived stages to be 3526 m/sec and 3527 m/sec,

Dead Sea Scrolls

McGregor Rocket Development Facility



“Black water shall elevate thy children to the heavens. Purify it. But thou shalt not combine it in a ratio greater than one kikkar to twenty shekkels, nor shalt thou burn rocks. Thus saith the lord.”



- Assumptions for Mission and Vehicle Sizing

| | |
|--------------------------|---------|
| HLLV T/W | 1.2 |
| 1st Stage Payload | 750 MT |
| RP-1 inert mass fraction | 0.06 |
| LH2 inert mass fraction | 0.08 |
| RP-1 Isp | 300 s |
| LH2 Isp | 420 s |
| RP O/F ratio | 2.27 |
| LH2 O/F ratio | 5.5 |
| Stage height, excluding | 36 m |
| RP-1 GLOM | 3040 MT |
| LH2 GLOM | 2060 MT |
| RP-1 Burnout time | 177 s |
| LH2 Burnout time | 205 s |
| RP-1 Stage diameter | 8.7 m |
| LH2 Stage diameter | 11.3 m |

| | |
|------------------------------------|-----------|
| SEP Isp | 2750 s |
| SEP thrust per engine | 1.08 N |
| Xenon tank mass fraction | 0.1 |
| SEP structural and margin mass | 0.1 |
| Solar Arrays and PPU mass fraction | 3.5 kg/kW |
| Low-thrust Delta V LEO to Phobos | 11.2 km/s |
| | |
| NTR Isp | 930 s |
| Delta V LEO to TMI | 4.2 km/s |
| Delta V TMI to MOC | 2.5 km/s |
| Delta V MOC to Phobos Capture | 0.4 km/s |
| NTR 15k lbf-thrust engine mass | 2600 kg |
| NTR tank mass fraction | 0.1 |
| Earth Aerocapture Delta V savings | 3.2 km/s |